

Constraints on the lunar core composition and thermal state from geophysical data and thermodynamic properties of liquid iron alloys

A. Rivoldini¹, M-H. Deproost¹, T. Van Hoolst¹, G. Morard², and H. Terasaki³

¹Observatoire Royal de Belgique, Belgique; ²Osaka University, Japan; ³Sorbonne Université, France

Constraints on the core of the Moon

- has liquid part (libration from LLR)
Williams 2001
- cooled fast enough to generate an early magnetic field
- radius 278-440 km and mean density **3900-6750 kg/m³** (seismic data, LLR, tides, induction)
... Garcia 2011; Williams 2014; Khan 2014; Matsumoto 2015, Matsuyama 2016
⇒ iron ($\rho_{\text{I-Fe}}=7400\text{kg/m}^3$) -rich alloy with a significant amount of light elements
- non candidate light elements: **Si** (unfavorable redox conditions), **O** and **H** (p too low during core-mantle differentiation)
- candidate light elements (formation conditions, bulk composition assumptions, chemical element partitioning between liquid metal and silicates):
S \leq 0.5wt% and **C \leq 5wt%**
... Dasgupta 2009; Chi 2014; Steenstra 2016,2017; Righter 2017

At 5GPa:

$\rho_{\text{Fe0.5wt\%S}} \sim 7300\text{kg/m}^3$ and $T_{\text{liquidus}} \sim 1950\text{K}$

$\rho_{\text{Fe5wt\%C}} \sim 7100\text{kg/m}^3$ and $T_{\text{liquidus}} \sim 1600\text{K}$

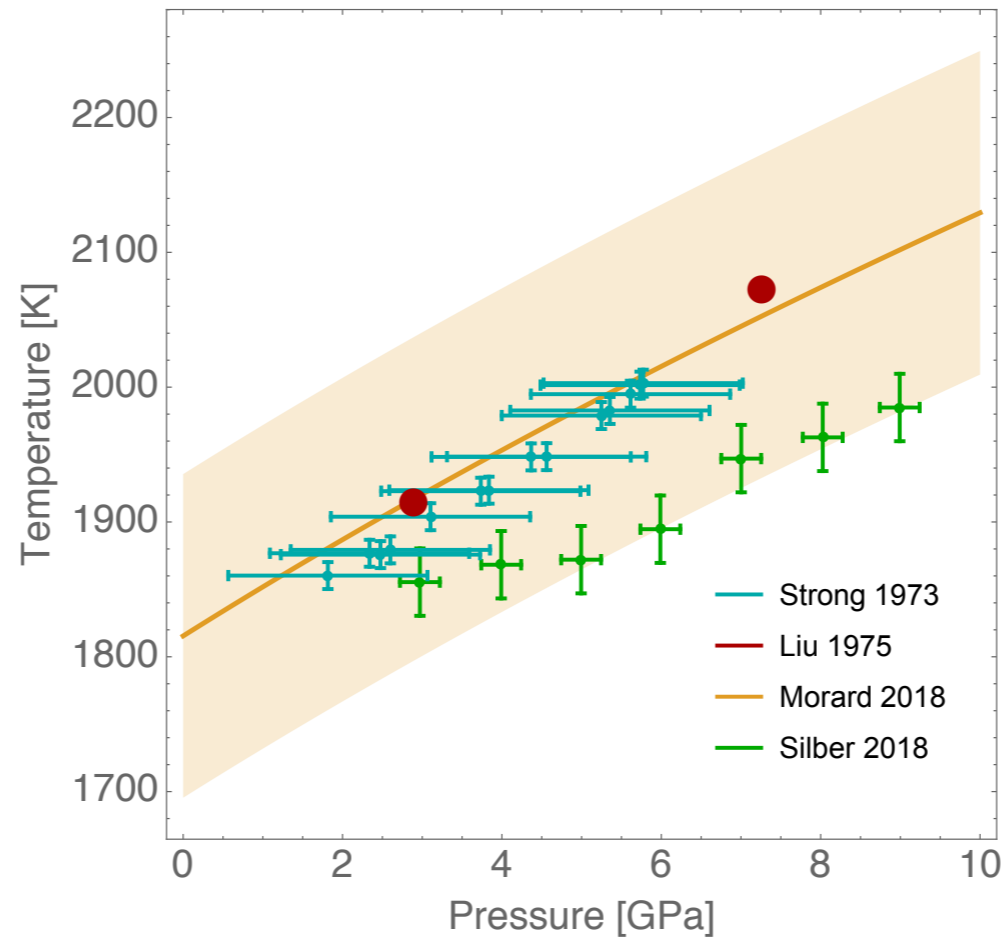
→ too dense to agree with core density inferences

⇒ need larger amounts of light elements

Core modeling

- iron-rich core can have a liquid and solid part
- radius of inner-core radius determined from liquidus temperature and core light element concentration
- need equations of state to compute relevant thermodynamic quantities for modeling interior structure and thermal evolution at relevant pressure and temperature conditions (e.g. density, thermal and chemical expansivity, heat capacity)
- equations of state and liquidus temperature of core alloys should be thermodynamically consistent

Fe liquidus

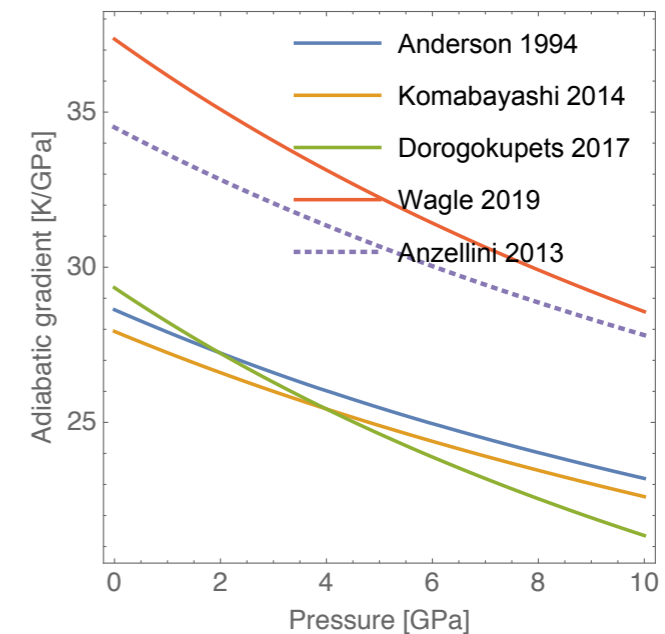
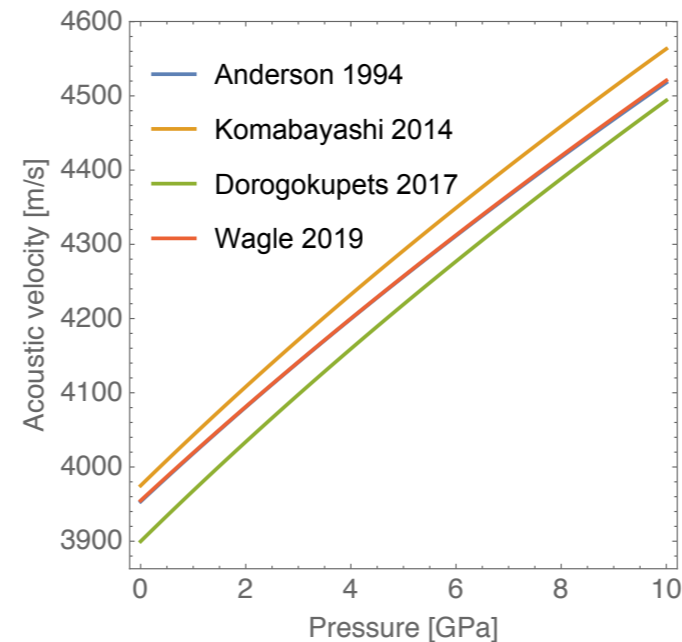
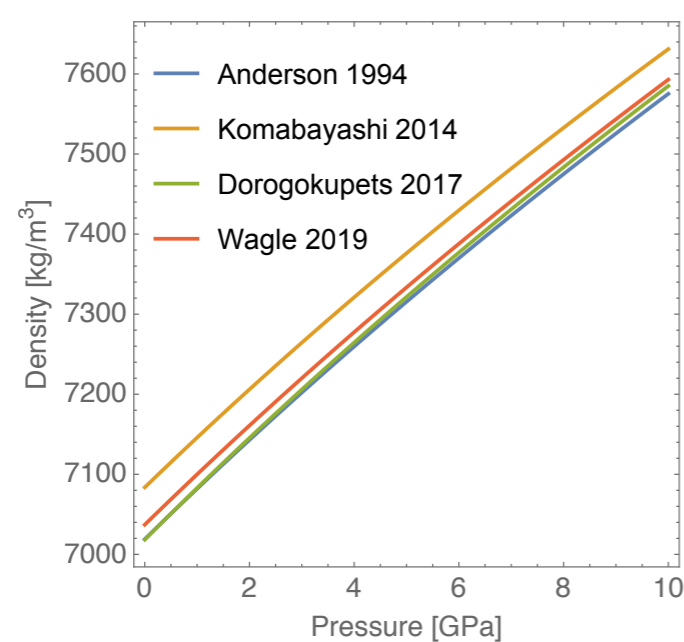


- liquidus deduced from high pressure data ($p > 10 \text{ GPa}$, Morard et al 2018) is in good agreement with low pressure experimental data (Strong 1973, Liu 1975)
- uncertainty on melting temperature at 1bar $\approx 10 \text{ K}$ and at 5GPa $\approx \mathbf{150 \text{ K}}$
- temperature increase along Moon core adiabat $\approx \mathbf{25 \text{ K}}$!

I-Fe equation of state

I-Fe eos are not derived from experimental data acquired at Moon core conditions:

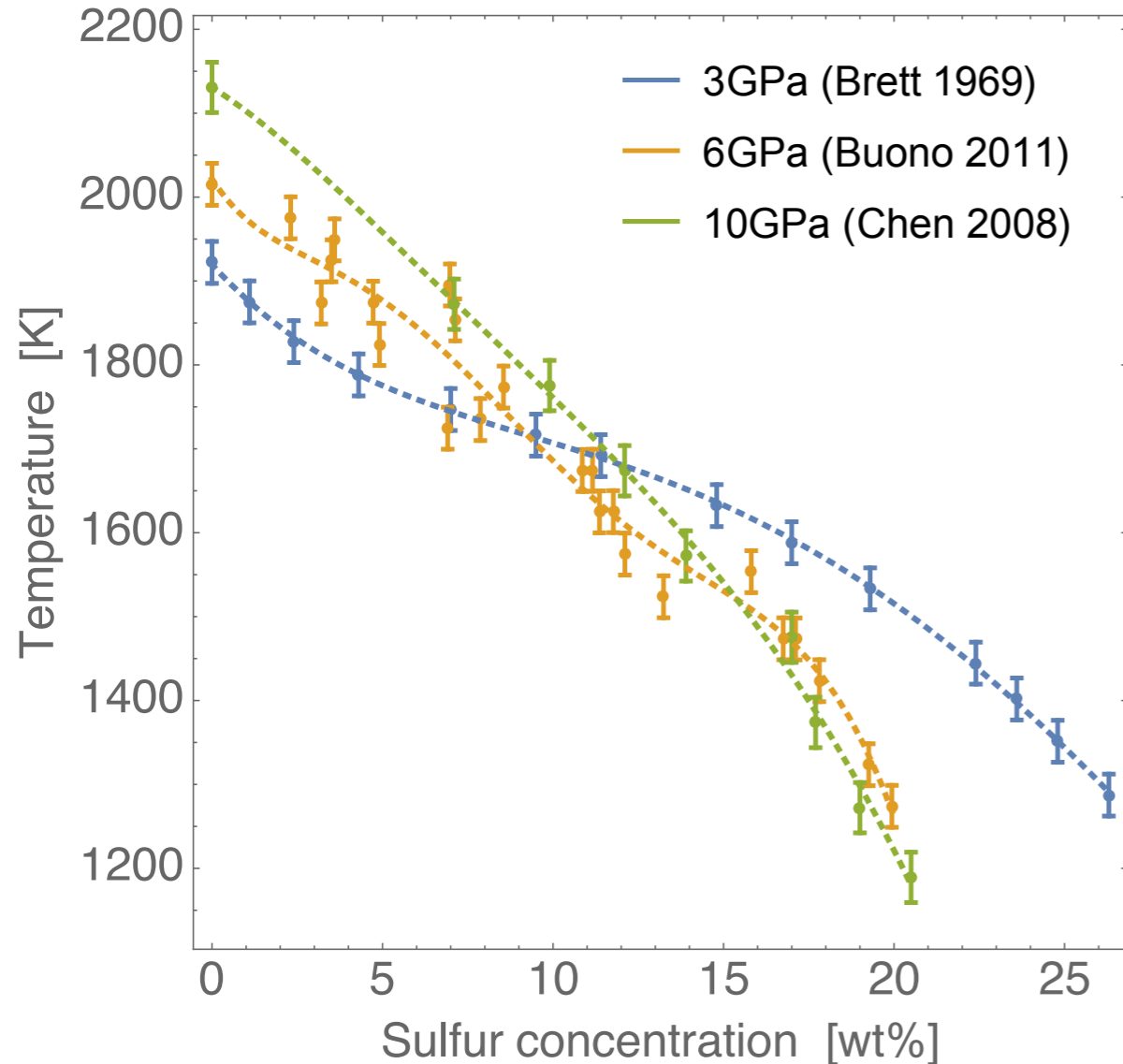
- Anderson et al 1994 (1bar thermoelastic data and 1000GPa shock data)
- Komabayashi 2014 (eos of fcc and hcp Fe and Fe liquidus from Anzellini 2013)
- Dorogokupets et al. 2017 (1bar thermoelastic data, eos of fcc and hcp Fe and Fe liquidus from Anzellini 2013)
- Wagle and Steinle-Neumann 2019 (Ab-Initio)



- along isentropes density differences are below 1% and acoustic velocity differences are below 2%
- but for thermal expansivity, heat capacity, and Grüneisen parameter the differences between the eos' can be quite larger
⇒ effect on core temperature
- all isentropes except that of Wagle et al. are less steep than the gradient along the Fe liquidus
⇒ bottom-up inner core growing for pure Fe and top-down for Wagle et al.
- all relevant thermodynamic quantities of I-Fe for structure and thermal evolution can be calculated from the eos'

Fe-S core model

Iron-rich liquidus



- highly non-ideal
- can be described with an asymmetric Margules model that has interaction parameters linear in p and T (Buono & Walker 2011)

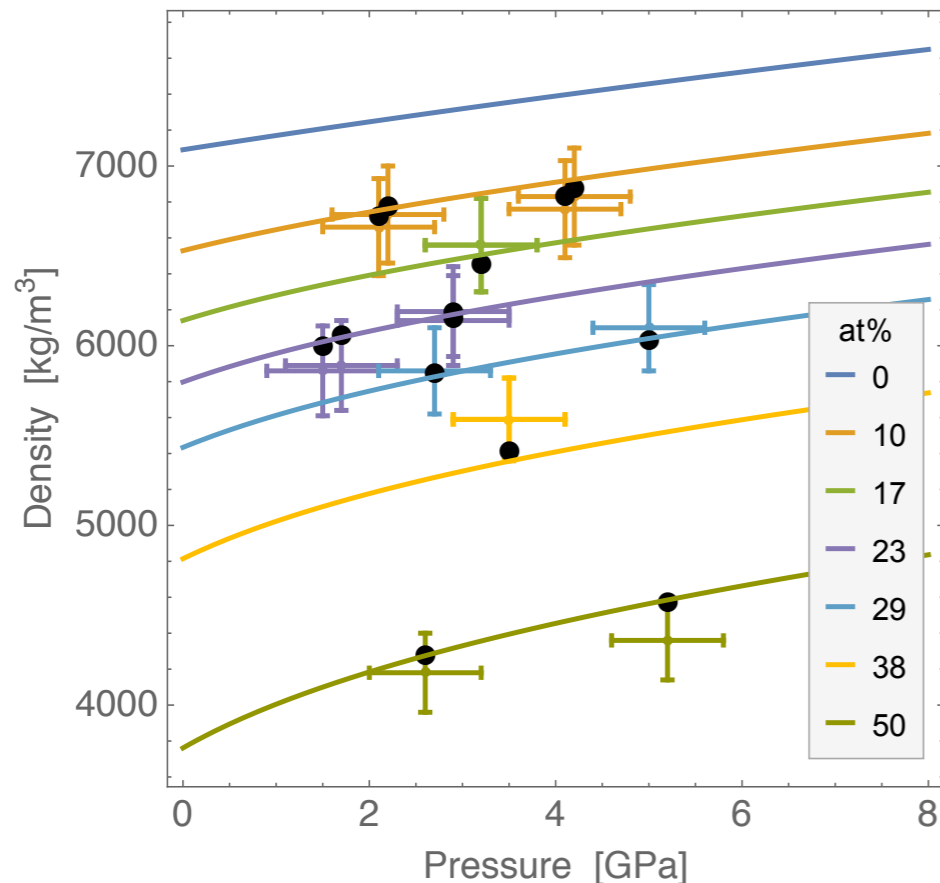
$$G^l(X_{\text{FeS}}, p, T) = (1 - X_{\text{FeS}}) G_{\text{Fe}}^l(p, T) + X_{\text{FeS}} G_{\text{FeS}}^l(p, T) +$$

$$(1 - X_{\text{FeS}}) RT \ln(1 - X_{\text{FeS}}) + X_{\text{FeS}} RT \ln(X_{\text{FeS}}) +$$

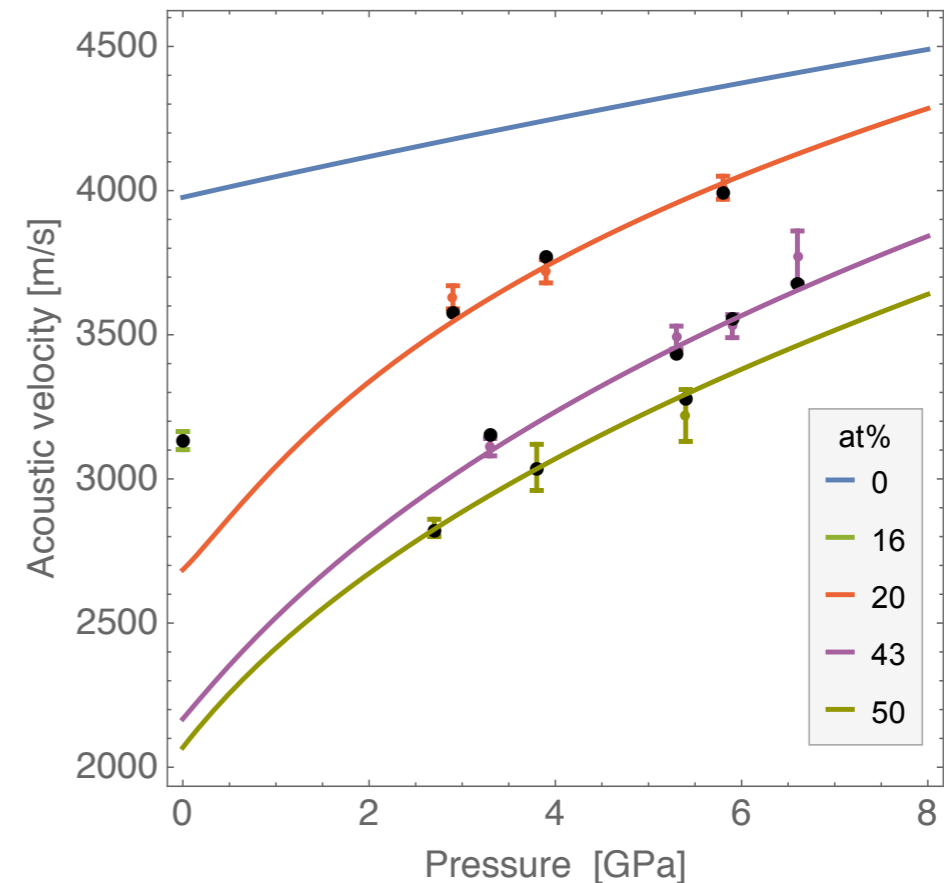
$$X_{\text{FeS}}(1 - X_{\text{FeS}}) [X_{\text{FeS}} W_{\text{Fe}}(p, T) + (1 - X_{\text{FeS}}) W_{\text{FeS}}(p, T)]$$

Elastic properties

Morard et al. 2018



Nishida et al. 2016



- densities of liquid Fe-S alloys at 5GPa in agreement with expected average Moon core density (3900-6750 kg/m³)
- Buono & Walker model induces a concentration dependent but (p,T) independent excessive mixing volume that can explain the high pressure density data
- **but not** the acoustic velocity data

Thermodynamic model

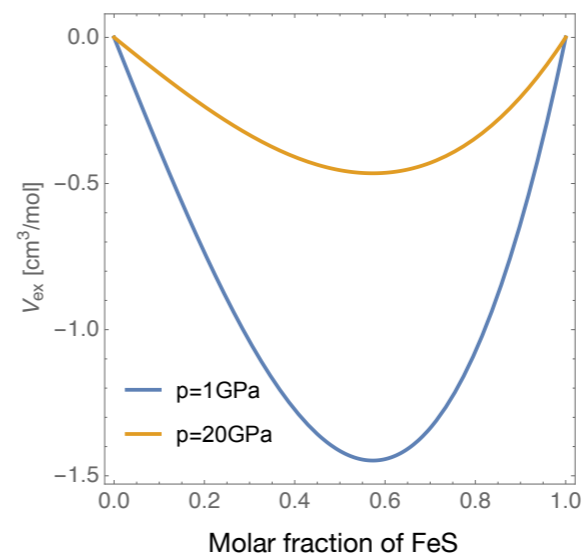
- end-members I-Fe (Komabayashi 2014) and I-FeS
- asymmetric Margules model with pressure dependent excessive volume

$$G_{\text{ex}}^I(X_{\text{FeS}}, p, T) = X_{\text{FeS}}(1 - X_{\text{FeS}}) [X_{\text{FeS}} W_{\text{Fe}}(p, T) + (1 - X_{\text{FeS}}) W_{\text{FeS}}(p, T)]$$

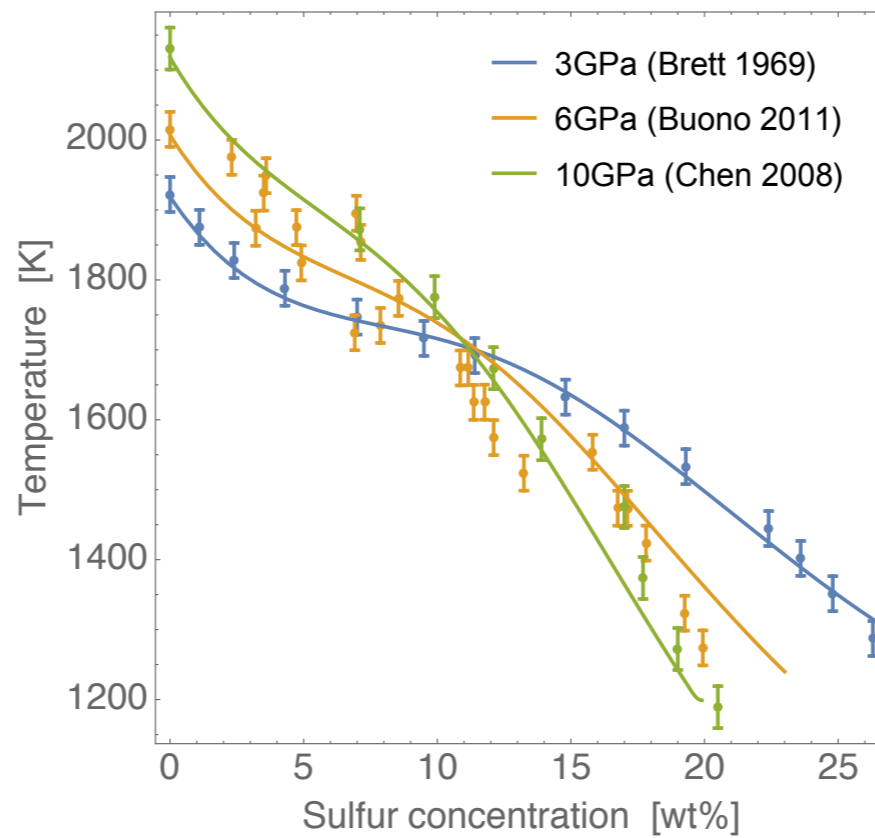
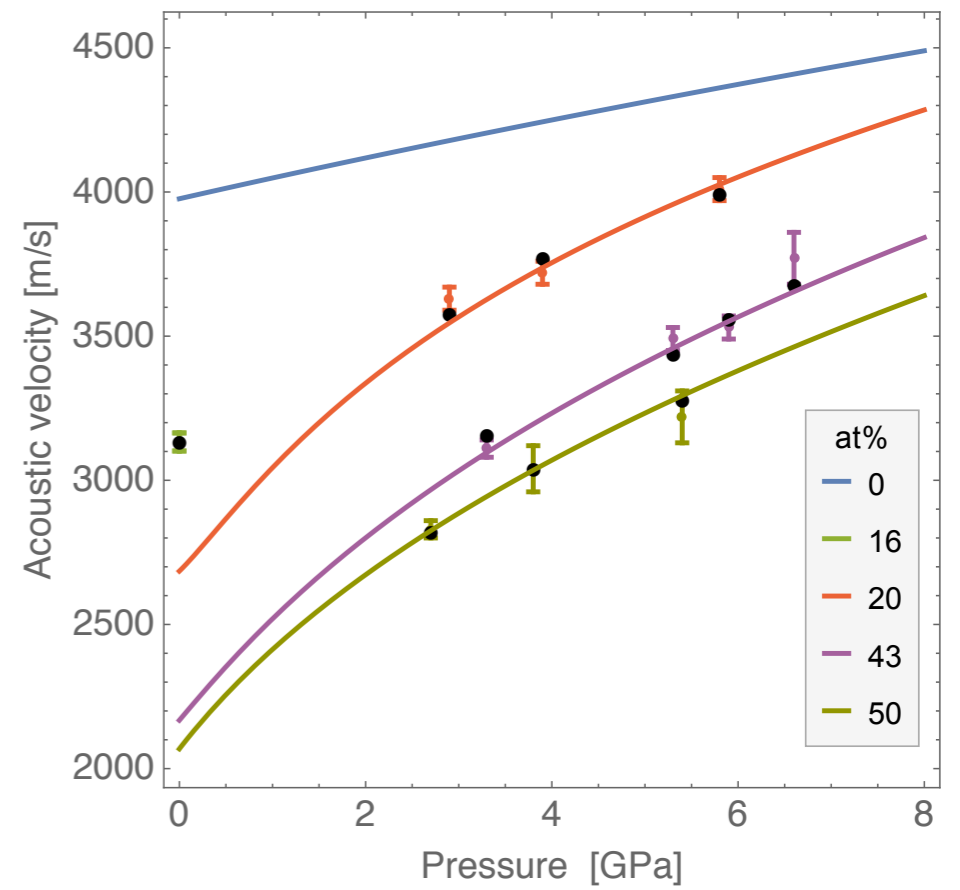
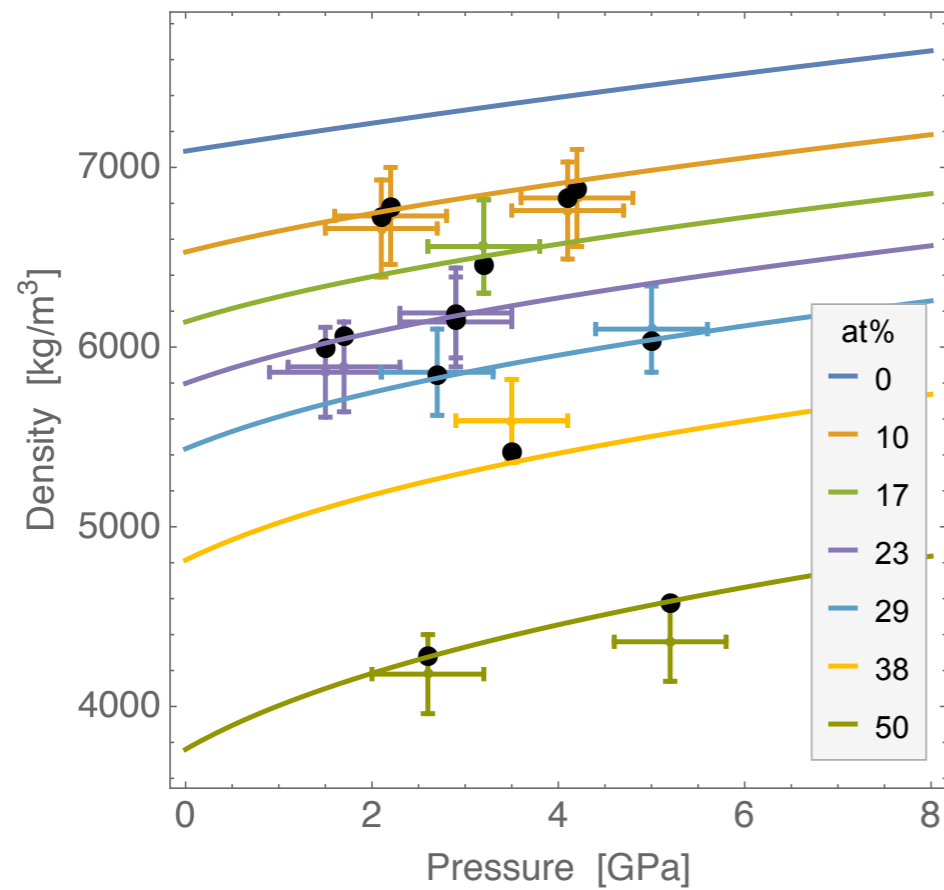
$$W_{\text{Fe}}(p, T) = W_{\text{Fe},H} - W_{\text{Fe},S}T + W_{\text{Fe},V} \int_0^p V_{\text{ex}}(p') dp'$$

$$W_{\text{FeS}}(p, T) = W_{\text{FeS},H} - W_{\text{FeS},S}T + W_{\text{FeS},V} \int_0^p V_{\text{ex}}(p') dp'$$

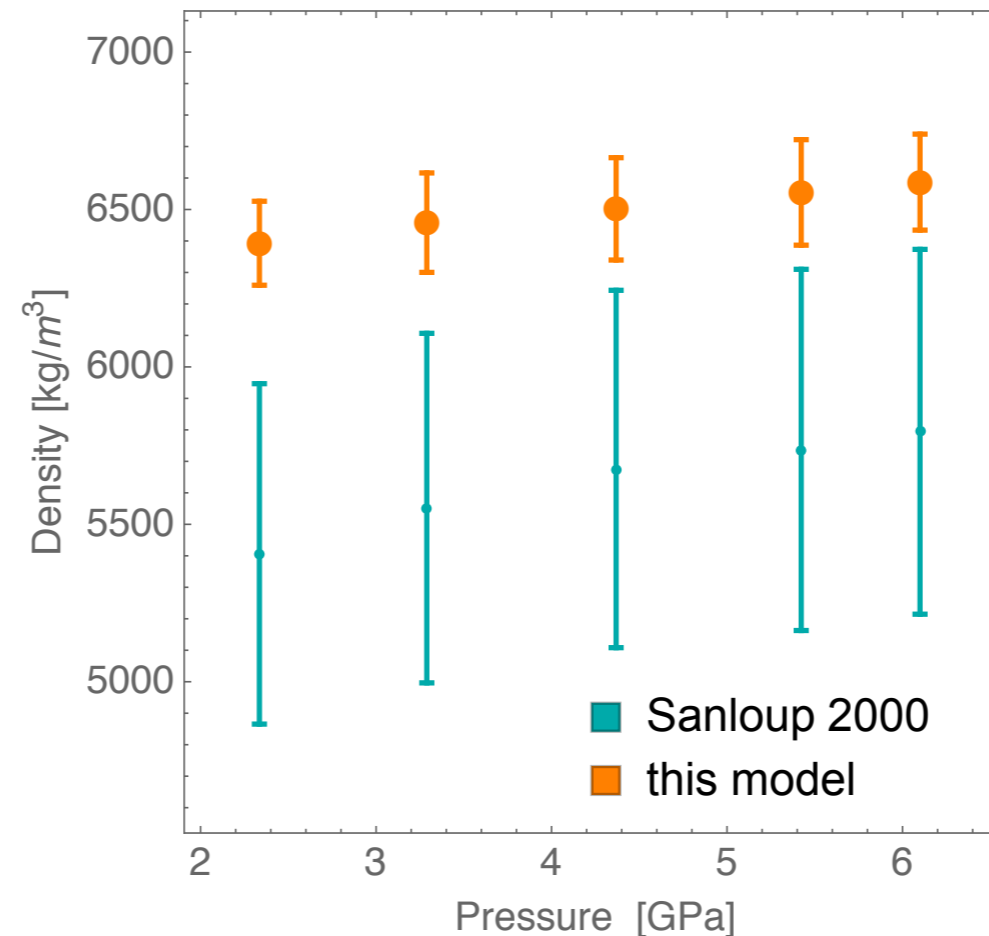
- EoS parameters for FeS (except ρ_{ref} and $\gamma=1.3$) (4) and interaction parameters (8) are estimated from liquidus, density, and acoustic velocity data
- ambient pressure density FeS from Kress 2007
- use pseudospinodal eos (Baonza 1995) for V_{ex}
→ V_{ex} decreases with increasing pressure



Data-Fit



Comparison with liquid Fe-10wt%S data used in several Moon core models

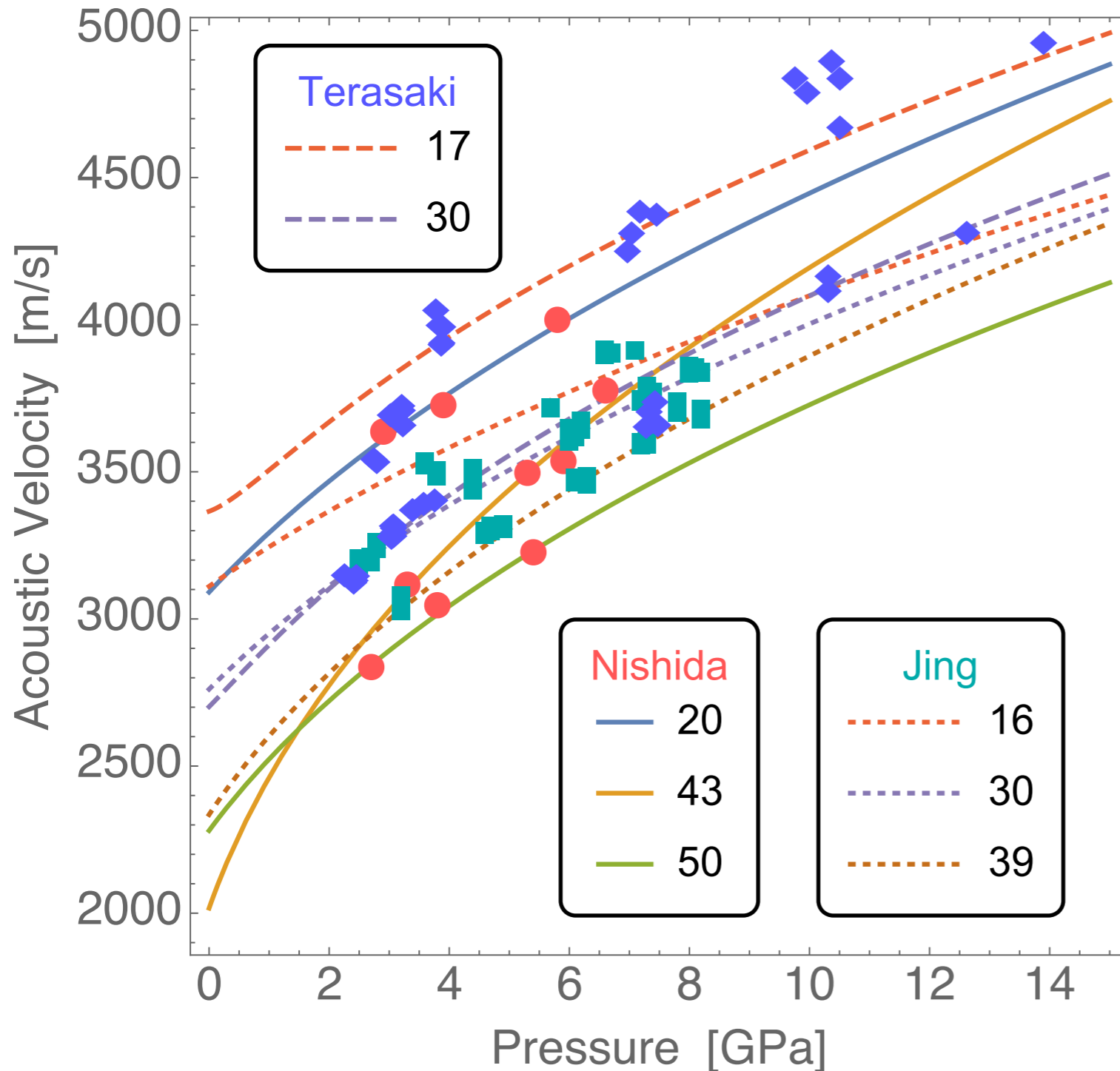


- uncertainty on elastic data induces errors on predicted densities of l-Fe-S alloys that are below 5% (taking into account correlations between eos parameters)
- predicted density of Fe-10wt%S is significantly larger than values reported by Sanloup et al. 2000 ⇒ new elastic data and thermodynamic model requires more sulfur to explain average core density

Caveats

- estimated model parameters depend on I-Fe eos
- results depend on reference density of FeS (Kaiura 1979, Kress 2007)
- cannot fit Grüneisen parameter from the data
- cannot assess model predictions for liquidus for compositions above the eutectic because of lack of experimental data
- thermodynamic Fe-S model very much dependent on used elastic data set

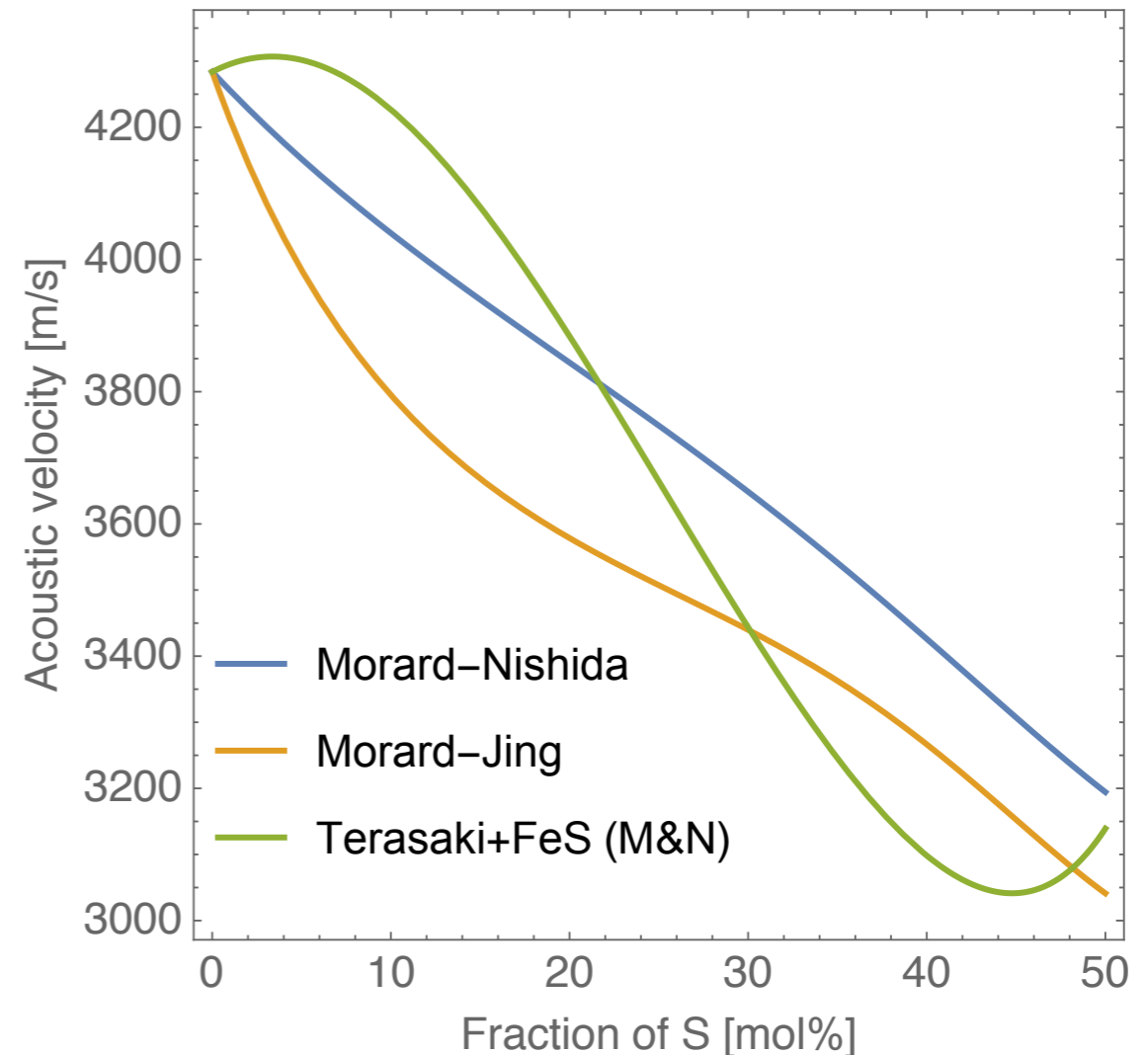
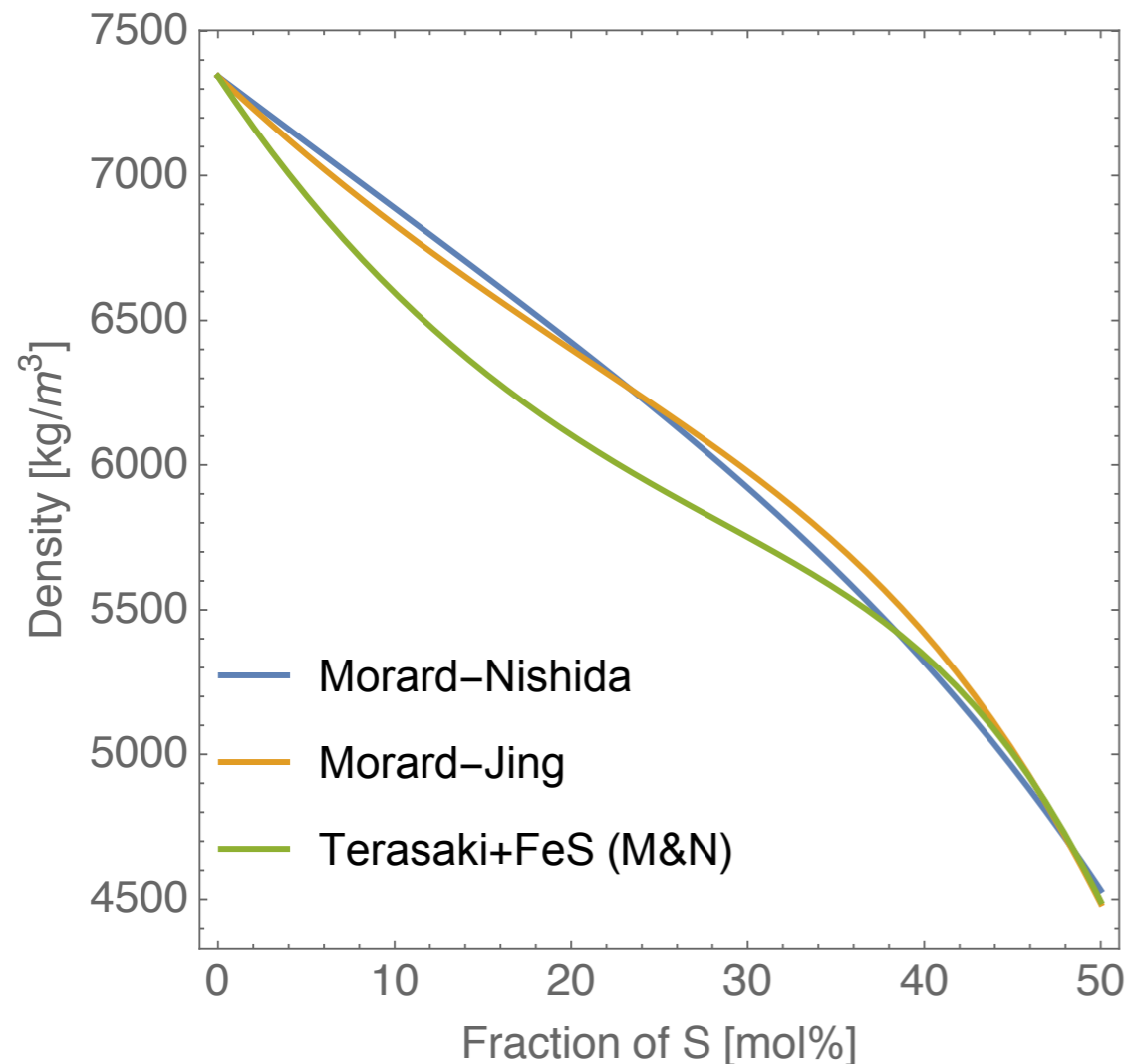
Acoustic velocity liquid Fe(Ni)-S



- Jing et al. 2014
Fe(16,30,39)at%S
- Nishida et al. 2016
Fe(20,43,50)at%S
- Terasaki et al. 201x
Fe10at%Ni(17,30)at%S
- weak dependence on temperature (curves are on isotherms 1900K)

⇒ **Inconsistency between different studies**

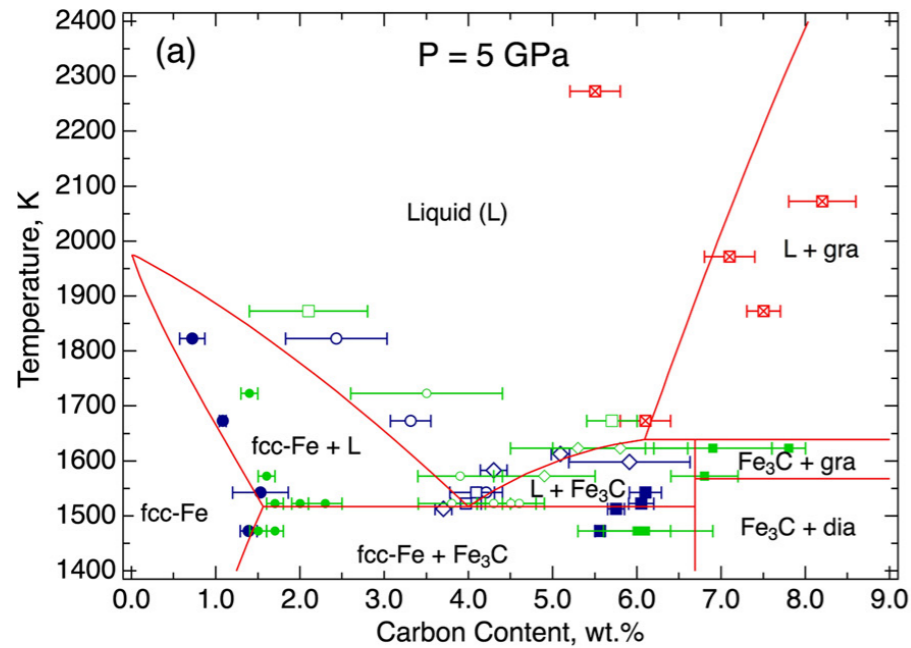
Effect of elastic data on thermodynamic model (5GPa, 2000K)



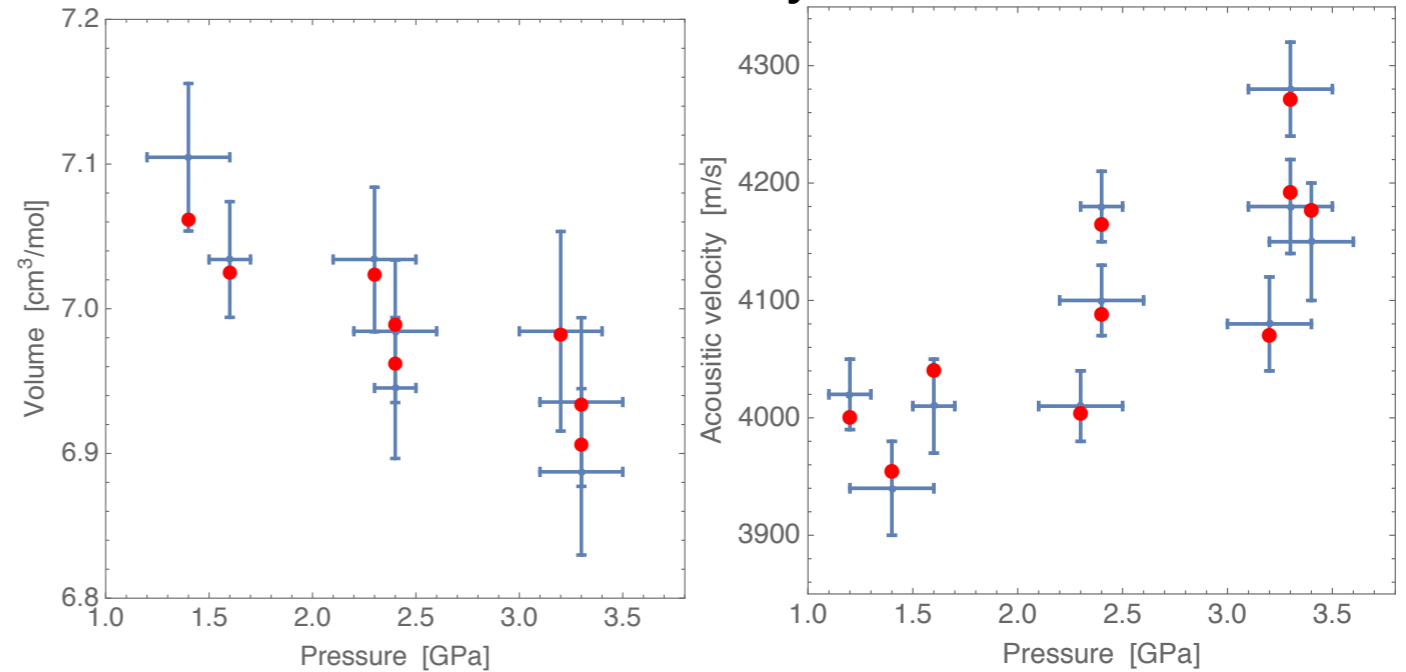
- density of liquid solution based on Morard 2018 density data depends weakly on acoustic velocity data
- but predicted acoustic velocities are quite different ...

Preliminary Fe-C core model

Fei and Brosh 2014



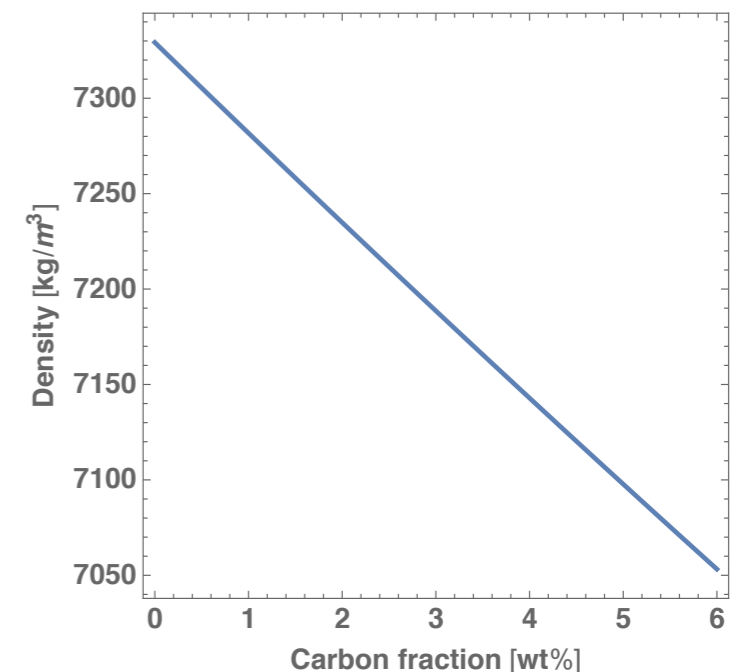
I-Fe3.5wt%C: Shimoyama et al. 2016



- at $\sim 5 \text{ GPa}$ C saturation in I-Fe $\approx 7 \text{ wt}\% \text{C}$
- assume ideal mixture of I-Fe (Komabayashi 2014) and I-Fe3.5wt%C (Shimoyama 2016)

\Rightarrow Density of liquid Fe-C significantly larger than **3900-6750 kg/m^3**

5 GPa, $T=2000\text{K}$

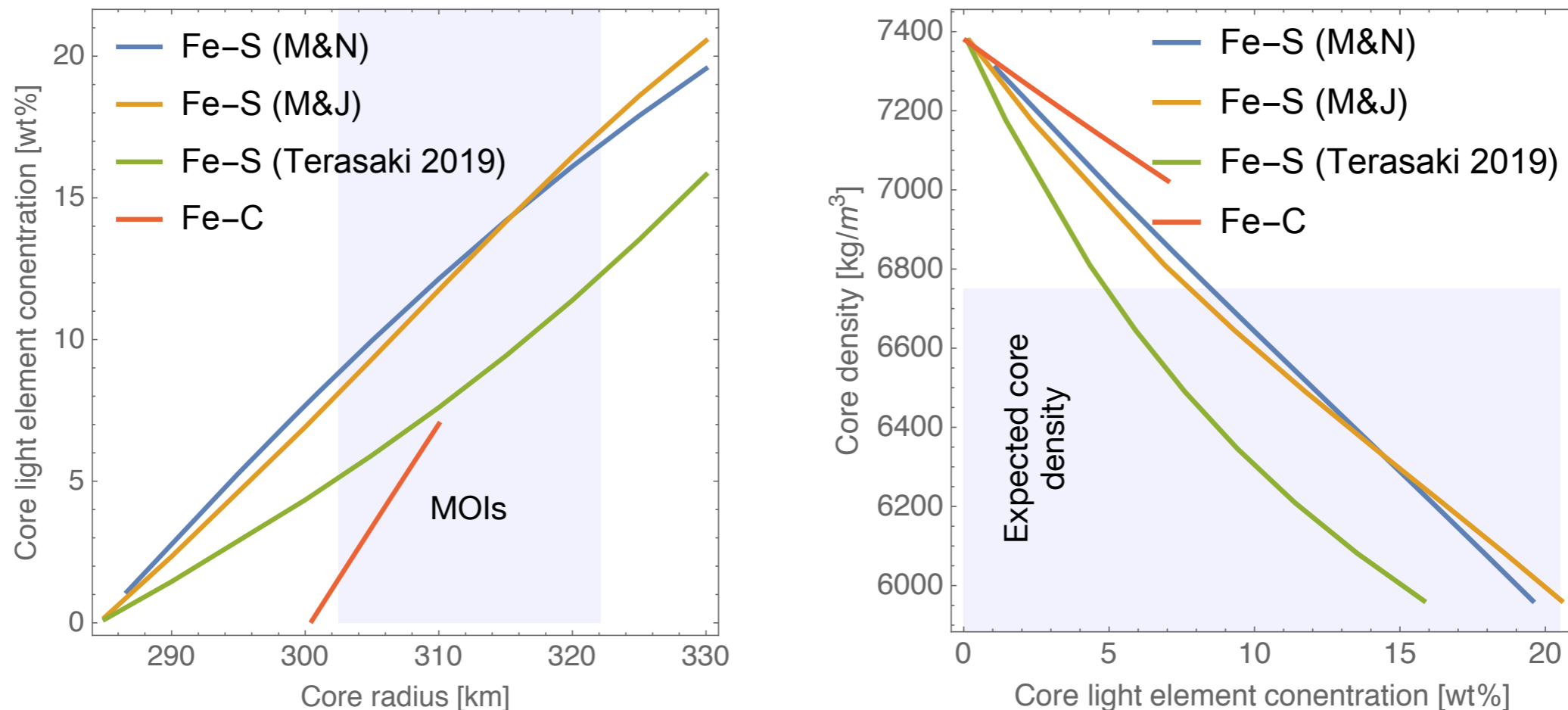


Moon models

- for illustration use the mantle density model of Weber et al. (2011)
- agree with the latest estimate of average shell moment of inertia (MOIs = 0.393112 ± 0.000012 , Williams et al., 2014)
- core thermal evolution model based on Davies et al. 2015 and mantle evolution model based on Morschhauser et al. 2011

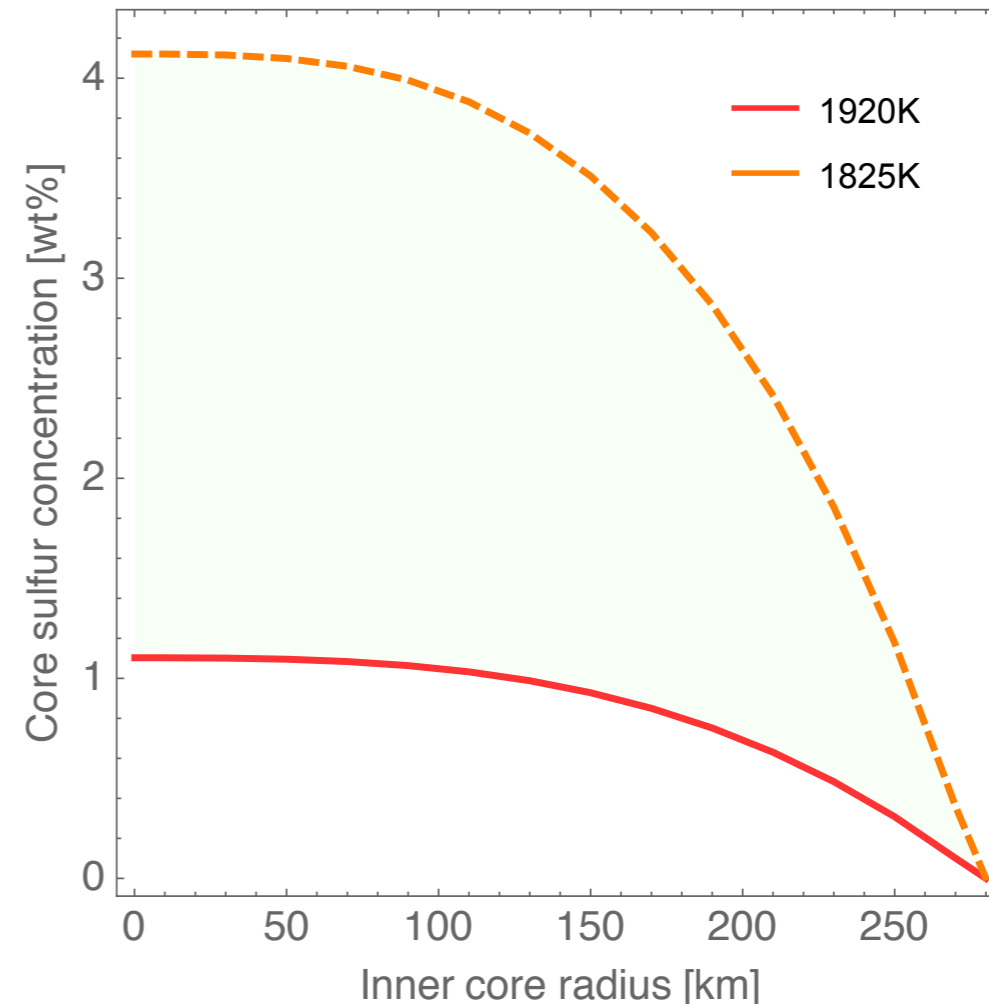
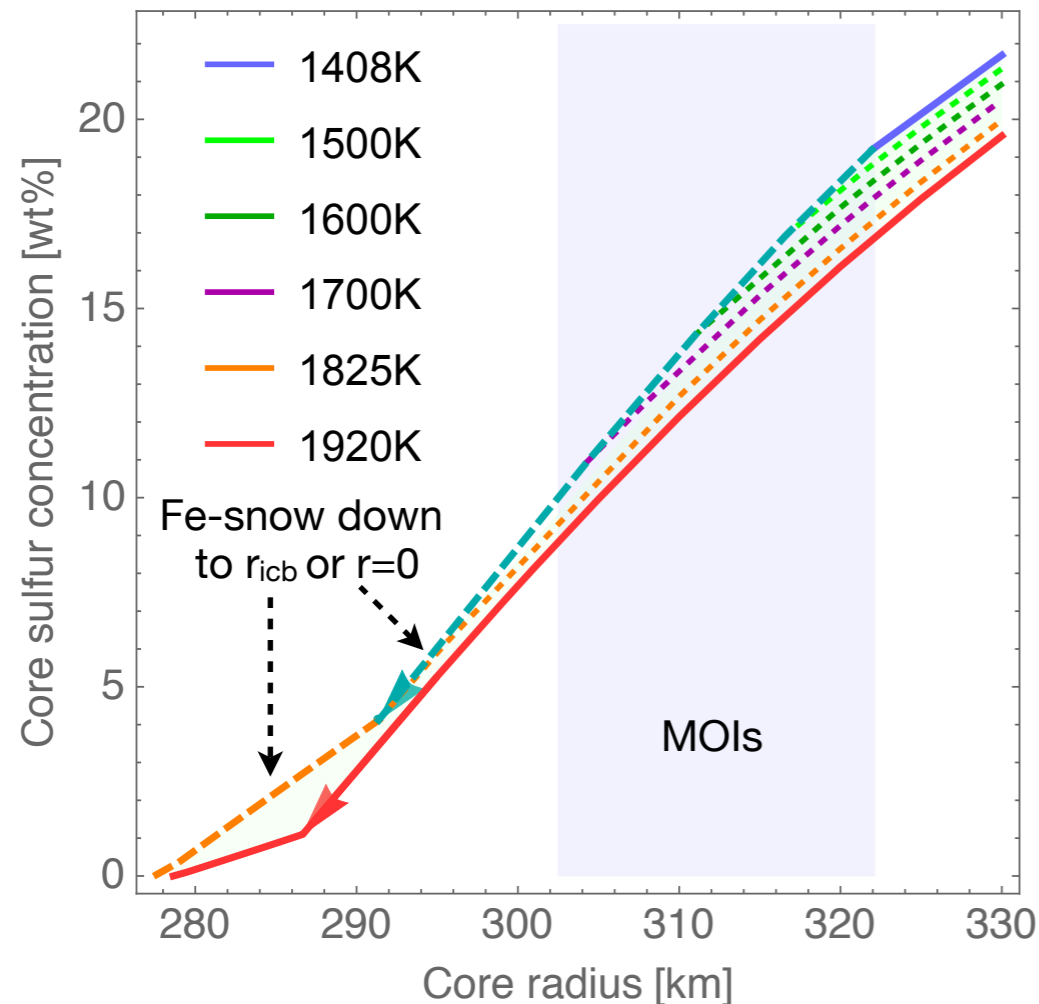
Structure functions: Fe-S and Fe-C

Core-mantle boundary Temperature: 1920K



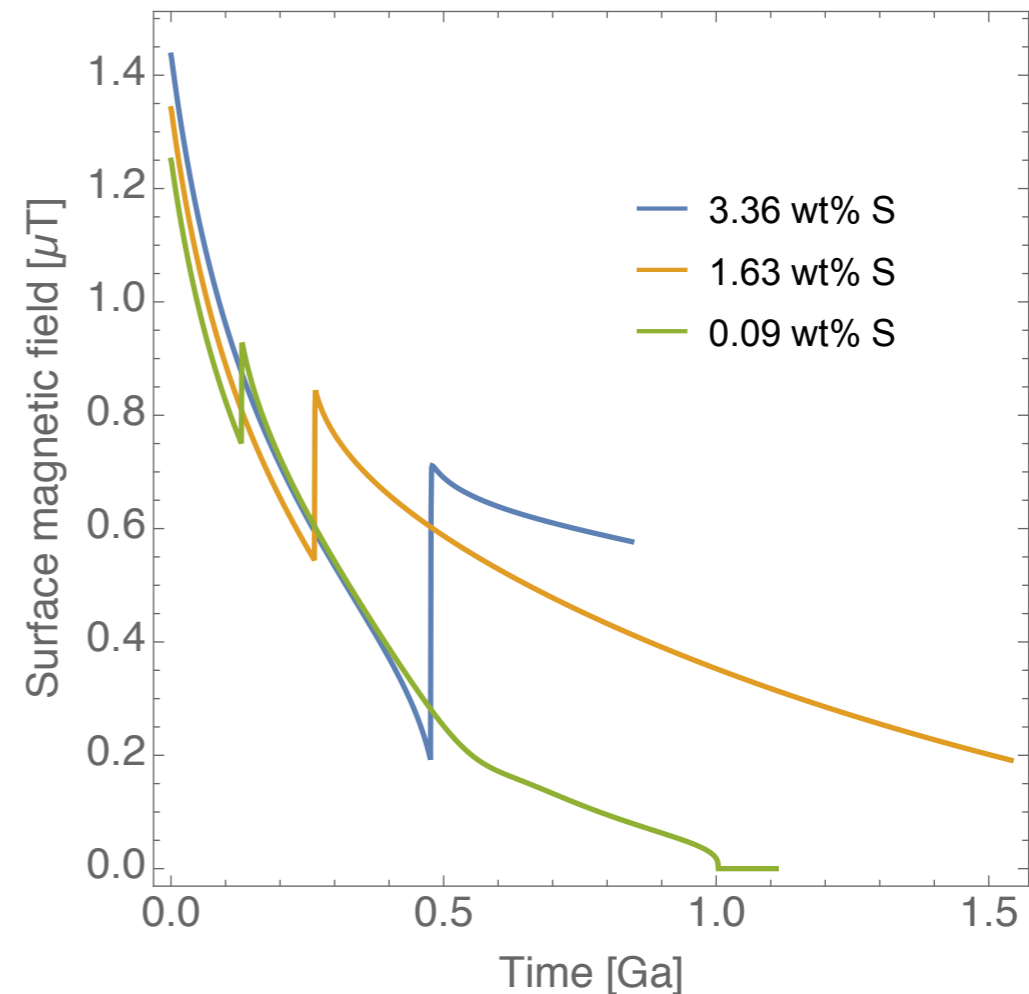
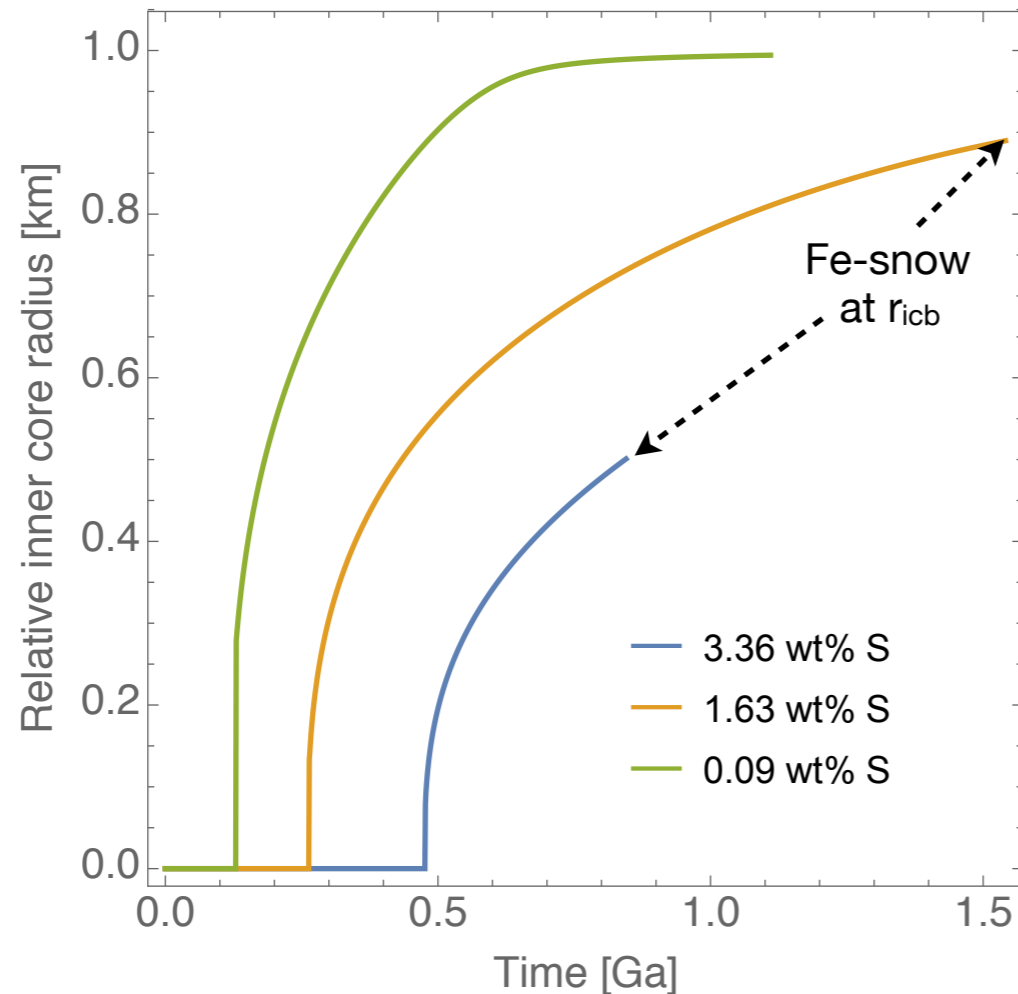
- the required amount of S to match the expected core density of the Moon is significantly larger than what is deduced from core formation models
- the weight fraction of C in liquid Fe-C is below 7wt% and the density of such an alloy is significantly above what is expected for the core of the Moon

Structure functions Fe-S (Morard-Nishida)



- models with the Weber et al. mantle cannot have an inner core (at 1σ)
- inner core possible if $r_{cmb} \lesssim 295\text{km}$ and $x_S \lesssim 5\text{wt}\%$
- bottom-up inner core growing requires $x_S \lesssim 4.2\text{wt}\%$
- to avoid present-day lower mantle melting $T_{cmb} \lesssim 1920\text{K}$ (Hirschmann et al. 2012)

Thermal evolution with bottom-up inner core formation

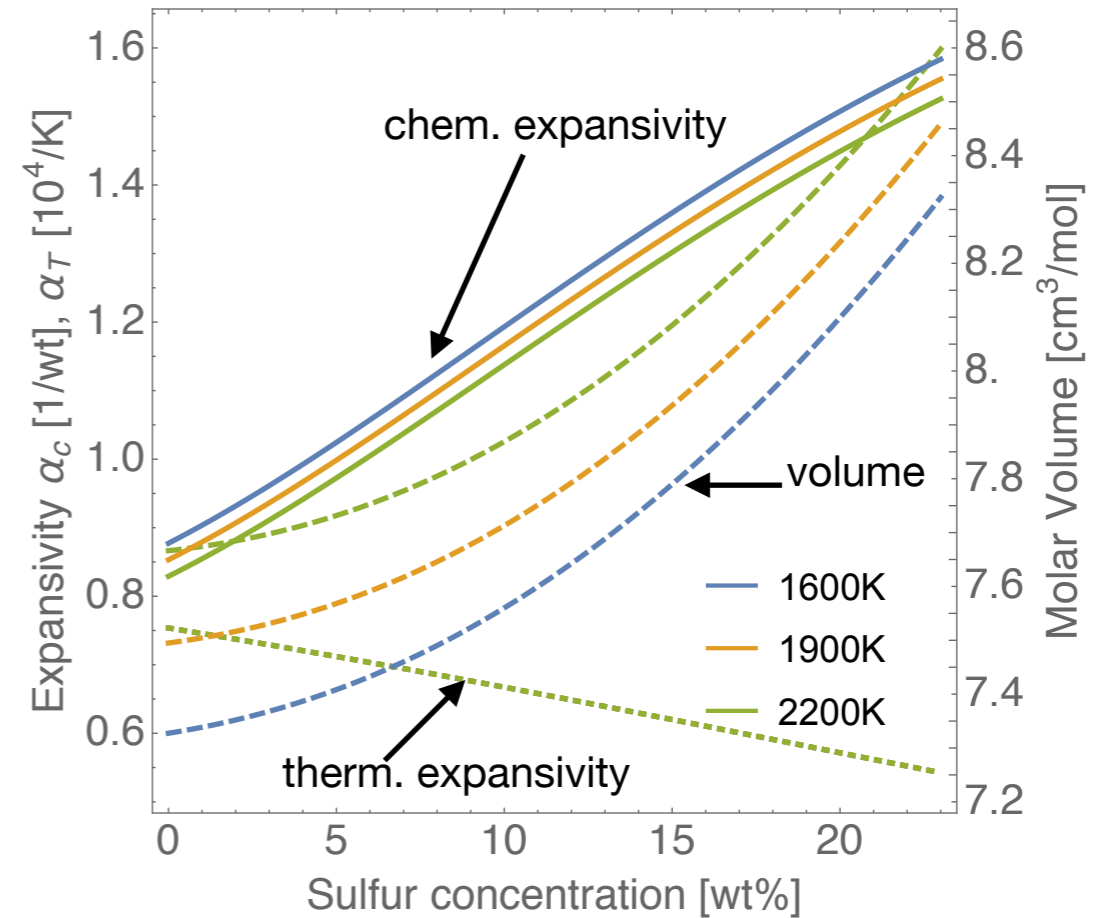
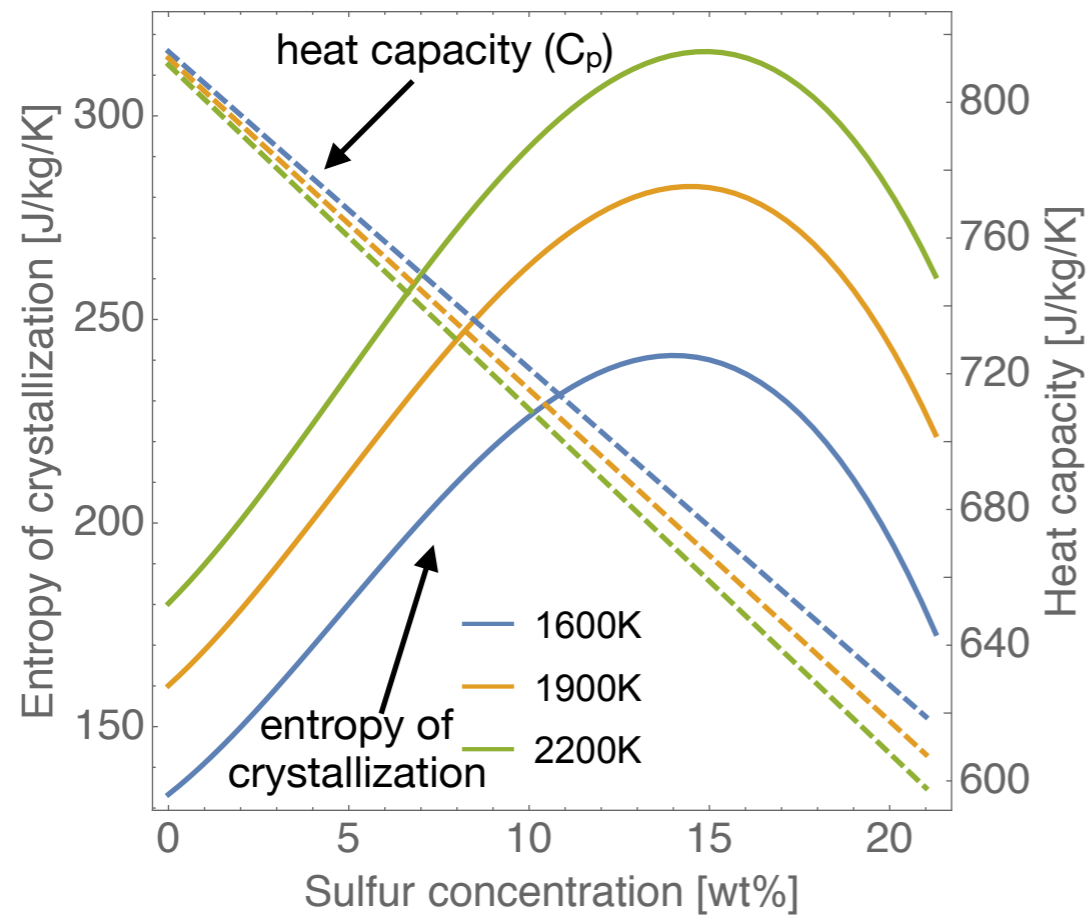


- all required thermodynamic quantities for core thermal evolution are computed from core model of this study (density, heat capacity, latent heat of crystallization, thermal- and chemical expansivity)
- main power and entropy source is latent heat
- timing of dynamo agrees with expected period of occurrence but predicted surface magnetic field is significantly below the 20-110 μT that are expected to explain the lunar magnetic records (Tikoo et al 2017)

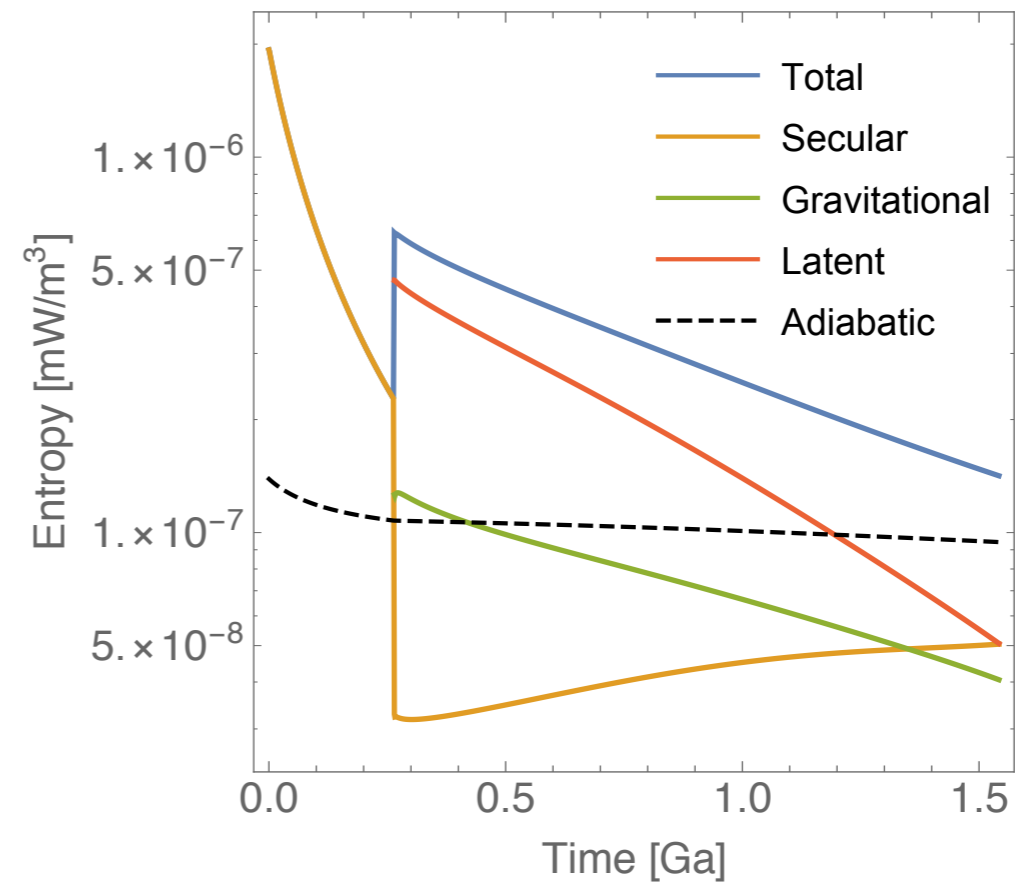
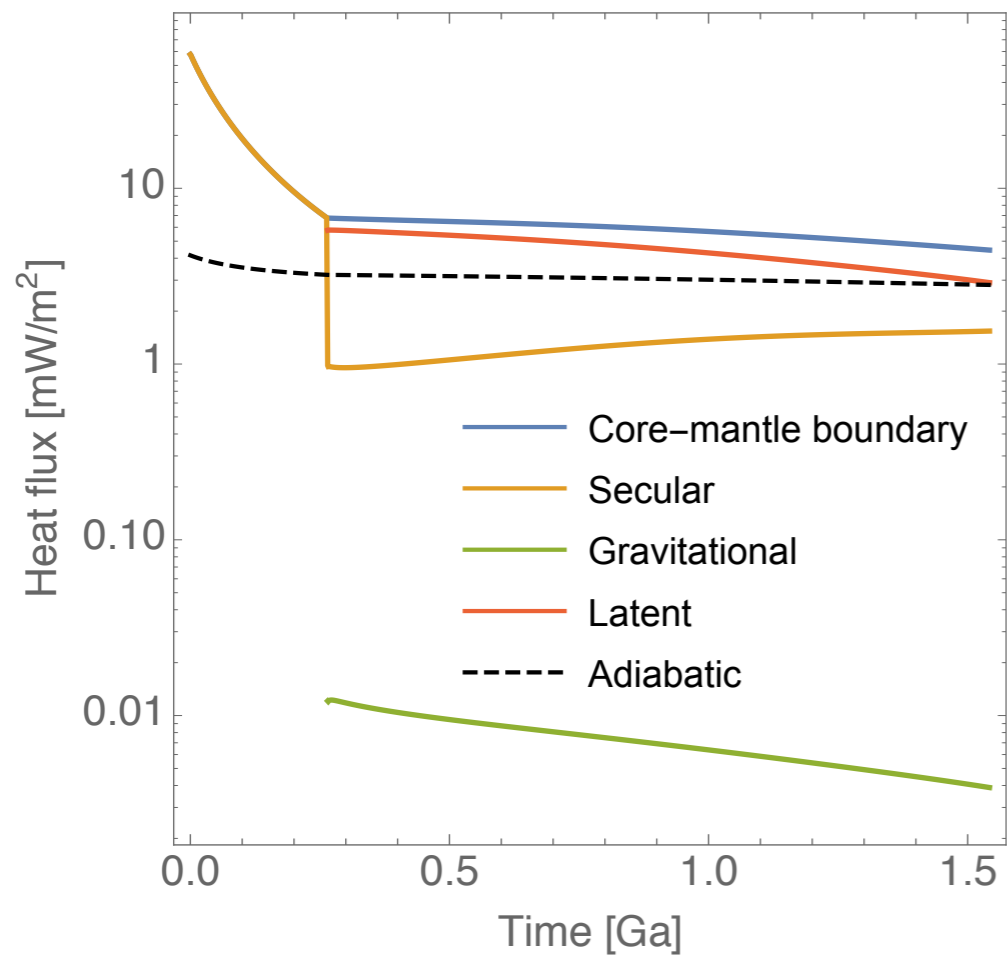
Conclusions

- melting data and new elastic data about Fe-S alloys can be described with a non-ideal mixing model that has a pressure dependent excess volume
- Fe-S models with an inner core and without a whole snowing liquid core cannot be much colder than $\sim 1825\text{K}$ and those models have less than $\sim 4.3\text{wt}\%$ of sulfur
- models with an inner-core agree with the timing of occurrence of the lunar dynamo but not with the expected field strength
- but the amount of S required to match the expected core density is too large to allow for bottom-up inner core formation and significantly above what is expected from core formation models
- C cannot be the only light element in the core because even at saturation concentration such a Fe-C alloy is denser than the expected Moon core density

Thermodynamic quantities



Thermal evolution

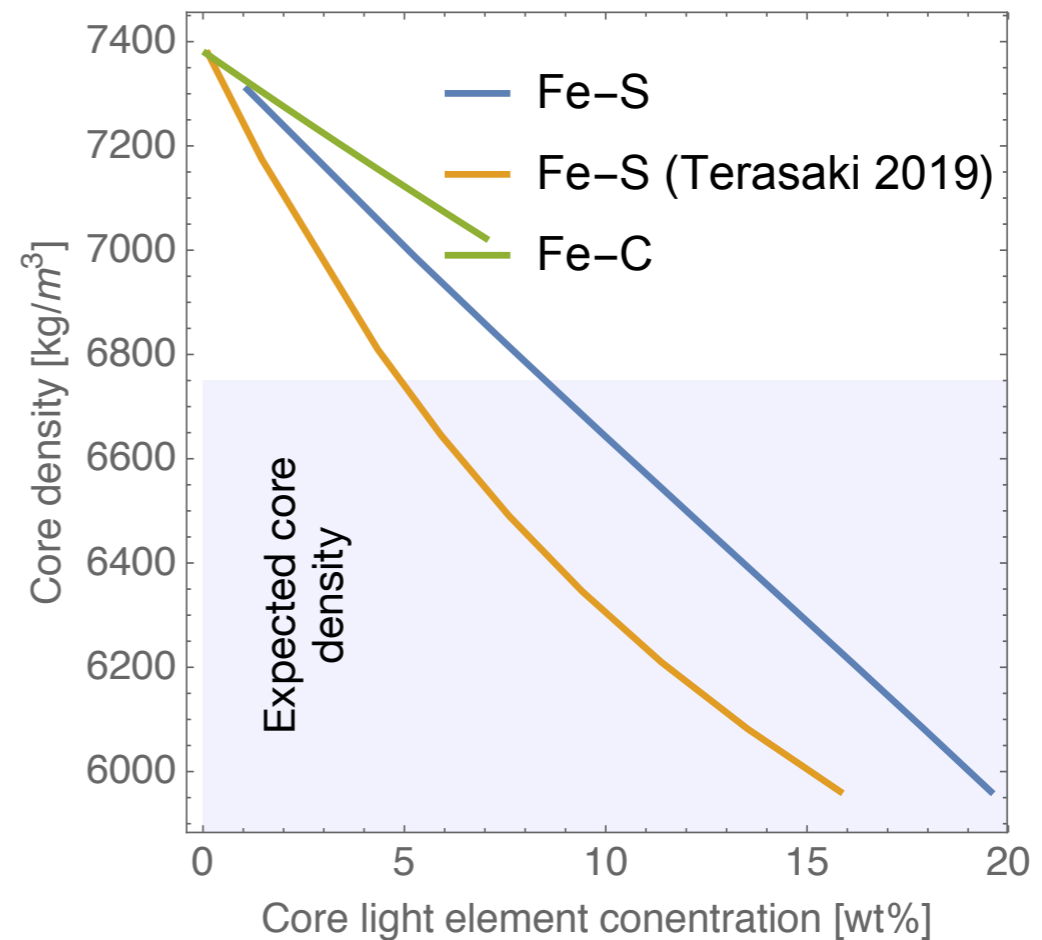
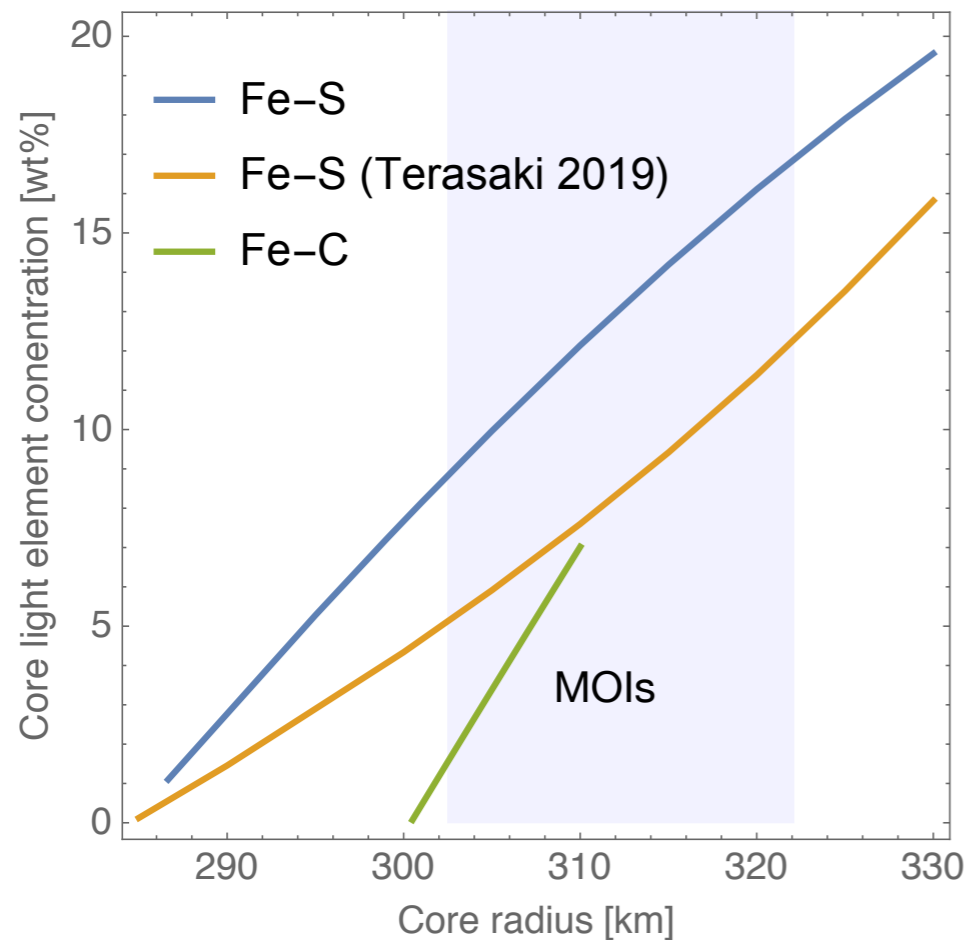


Core composition

- Steenstra 2016
depletion of siderophiles elements in the core can be explained if $S > 8\text{wt}\%$
but S abundance in mantle implies S poor core
but V and Cr abundances require either a S poor core with a differentiation temperature $> 3100\text{K}$ but core mass $\sim 2.5\text{wt}\%$ (my models $< 1.3\text{wt}\%$) or $S \sim 8.5\text{wt}\%$ with $T_{\text{diff}} \sim 2200\text{K}$
difficult to explain anything with $m_{\text{Core}} < 2.3\text{wt}\%$
- Steenstra 2017
to explain observed S, Se, Te in silicate Moon requires fully molten Moon at core-mantle equilibration
- Steenstra 2017
metal-silicate partitioning of C, S, Ni and BSM (are they reliable?) abundances of S and C
 $S < 0.16\text{wt}\%$, main light element carbon up to $\sim 4.8\text{wt}\%$
- Righter 2017

Structure functions: Fe-S and Fe-C

Core-mantle boundary Temperature: 1920K



- models based on elastic data of Terasaki et al 2019 require less sulfur at a given core radius to explain the density of the core
- C weight fraction in liquid Fe-C is below 7wt% and
- core densities of Fe-C models are significantly larger than the expected core density of the Moon